## ARTICULAR-EMINENCE MEASUREMENTS PERFORMED BY CONVENTIONAL AND THREE-DIMENSIONAL METHOD

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## PURPOSE

Articular eminence (AE) morphology could be expressed by dimensions and angles measured by different methods. The aim of this study was to compare conventional two-dimensional with threedimensional laser method.

## MATERIALS AND METHODS

The study was carried out on 20 human dry skulls ( 18 to 65 years) from medieval and contemporary period. Measurements were performed on sections (real and virtual) through the AE silicone impressions (lateral-medial) using two-dimensional and threedimensional (laser) digitalization. First section was the most lateral section through the silicone impression. AE inclination (first method (M1) "fossa roof - eminence top" and second method (M2) "best fit line" method) in relation to the Frankfurt horizontal, AE height and the length of curved line (highest to the lowest AE point) were measured (Figures 1-6). Results were statistically analyzed with significance level of 0.05


Figure 1. AE inclination measurement by conventional (two-dimensional) method in VistaMetrix software.


Figure 3. AE height measurement by conventional (twodimensional) method in VistaMetrix software.


Figure 2. AE inclination measurement by conventional (two-dimensional) method in VistaM Metrix software.


Figure 4. AE curved line length measurement by
conventional (two-dimensional) method in VistaMetri conventional (two-dimensional) method in VistaMetrix
software.


Figure 6. AE measurements on virtual sections through the three-dimensional laser scan of AE silicone impression.

## RESULTS

Although small differences existed between AE measurements performed by conventional and threedimensional laser technology, most of obtained differences (Tables 1-10) were not statistically significant (p values: AE inclination 0.003 to 1.0 ; AE height 0.012 to 1.0 ; curved line length of 0.115 to 1.0 ). Differences between AE inclination values measured by "best fit line" method and "fossa roof - eminence top" method were statistically significant ( $\mathrm{p}<0.001$ ).

|  |  | ariables | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline 11 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 30,230 | 4,430 | 0,824 |
|  |  | LASER | 20 | 30,250 | 4,590 |  |
|  | $\begin{gathered} \hline 12 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 47,610 | 5,240 | 0,167 |
|  |  | LASER | 20 | 47,890 | 5,490 |  |
|  | $\begin{gathered} \mathrm{HR} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 5,280 | 1,160 | 1,000 |
|  |  | LASER | 20 | 5,270 | 7,540 |  |
|  | $\begin{aligned} & \hline \mathrm{LR} \\ & (\mathrm{~mm}) \end{aligned}$ | CONVENTIONAL | 20 | 10,770 | 1,550 | 0,115 |
|  |  | LASER | 20 | 10,830 | 13,470 |  |

Table 2. Statistical parameters of AE measurements on second section, right (N-number of specimens; SD-standard deviation; $p-\mathrm{p}$ value; 11-AE inclination, first method; 12 -AE inclination, second method; $H$-AE height, $L$-AE curved line length, $R$-right side).

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline 11 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 33,800 | 3,930 | 0,503 |
|  |  | LASER | 20 | 33,830 | 4,050 |  |
|  | $\begin{gathered} 12 R \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 54,350 | 10,420 | 0,012* |
|  |  | LASER | 20 | 54,520 | 10,270 |  |
|  | $\begin{gathered} \hline \mathrm{HR} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 6,520 | 1,020 | 0,115 |
|  |  | LASER | 20 | 6,570 | 0,960 |  |
|  | $\begin{aligned} & \hline \mathrm{LR} \\ & (\mathrm{~mm}) \end{aligned}$ | CONVENTIONAL | 20 | 12,420 | 1,650 | 0,824 |
|  |  | LASER | 20 | 12,520 | 1,660 |  |

Table 3. Statistical parameters of AE measurements on third section, right ( $N$-number of
specimens; SD-standard deviation; $p-\mathrm{p}$ value; $11-\mathrm{AE}$ inclination, first method; $12-\mathrm{AE}$ inclination, second method; $H$-AE height, $L$-AE curved line length, $R$-right side).

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline 1 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 35,410 | 4,440 | 1,000 |
|  |  | LASER | 20 | 35,100 | 4,190 |  |
|  | $\begin{gathered} \hline 12 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 57,270 | 10,330 | 0,115 |
|  |  | LASER | 20 | 57,250 | 10,470 |  |
|  | $\begin{aligned} & \hline \text { HR } \\ & (\mathrm{mm}) \end{aligned}$ | CONVENTIONAL | 20 | 7,300 | 1,050 | 0,263 |
|  |  | LASER | 20 | 7,230 | 1,030 |  |
|  | $\begin{gathered} \stackrel{\mathrm{LR}}{(\mathrm{~mm})} \end{gathered}$ | CONVENTIONAL | 20 | 13,340 | 1,170 | 0,503 |
|  |  | LASER | 20 | 13,360 | 1,140 |  |

Table 4. Statistical parameters of AE measurements on fourth section, right $(\mathbb{N}$-number of
specimens; $S \mathrm{SD}$-standard deviation; $\mathrm{p}-\mathrm{p}$ value; $11-\mathrm{AE}$ inclination, first method; $12-\mathrm{AE}$ inclination specimens; SD-standard deviation; $p-\mathrm{p}$ value; 11 -AE inclination, first method; 12 -AE inclination second method $H$-AE height, $L$

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 11 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 34,400 | 4,760 | 0,824 |
|  |  | LASER | 20 | 34,440 | 4,610 |  |
|  | $\begin{gathered} \hline 12 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 57,940 | 8,710 | 0,263 |
|  |  | LASER | 20 | 57,580 | 9,520 |  |
|  | $\begin{gathered} \mathrm{HR} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 7,080 | 1,000 | 0,167 |
|  |  | LASER | 20 | 7,020 | 0,950 |  |
|  | $\begin{aligned} & \hline \mathrm{LR} \\ & (\mathrm{~mm}) \end{aligned}$ | CONVENTIONAL | 20 | 13,180 | 1,440 | 1,000 |
|  |  | LASER | 20 | 13,170 | 1,390 |  |

Table 5. Statistical parameters of AE measurements on fifth section, right ( $N$-number of specimens; SD-standard deviation; $p-p$ vealue; $11-A E$ inclination, first method; 12 -AE inclination, second method; $H$-AE height, $L$-AE curved line length, $R$-right side).

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline 11 \mathrm{R} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 33,470 | 5,540 | 0,824 |
|  |  | LASER | 20 | 33,440 | 5,580 |  |
|  | $\begin{gathered} 12 R \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 53,450 | 9,590 | 0,041* |
|  |  | LASER | 20 | 53,680 | 9,590 |  |
|  | HR <br> (mm) | CONVENTIONAL | 20 | 6,030 | 1,180 | 0,041* |
|  |  | LASER | 20 | 6,190 | 1,240 |  |
|  | $\begin{gathered} \hline \mathrm{LR} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 11,970 | 1,640 | 0,503 |
|  |  | LASER | 20 | 11,860 | 1,590 |  |

Table 6. Statistical parameters of $A E$ measurements on first section, left ( $N$-number of specimens; SD-standard deviation; p-p value; 11-AE inclination, first method; 12 -AE inclination,

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 11 \mathrm{~L} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 33,020 | 4,320 | 0,824 |
|  |  | LASER | 20 | 33,110 | 4,510 |  |
|  | $\begin{gathered} \hline 12 \mathrm{~L} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 50,040 | 7,780 | 0,041* |
|  |  | LASER | 20 | 50,240 | 7,900 |  |
|  | HL (mm) | CONVENTIONAL | 20 | 5,760 | 0,960 | 0,263 |
|  |  | LASER | 20 | 5,750 | 1,170 |  |
|  | $\begin{gathered} \mathrm{LL} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 11,120 | 2,190 | 1,000 |
|  |  | LASER | 20 | 11,130 | 2,290 |  |

Table 7. Statistical parameters of AE measurements on second section, left ( $N$-number of specimens; SD-standard deviation; $p-\mathrm{p}$ value; 11 -AE inclination, first method; 12 -AE inclination, second method: H-AE height, L-AE curved line length, L-efft side).

| $\begin{aligned} & \text { ㅇㅡㅡ } \\ & \text { 은 } \end{aligned}$ |  | ariables | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{I} 1 \mathrm{~L} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 33,680 | 5,060 | 0,041* |
|  |  | LASER | 20 | 33,940 | 5,060 |  |
|  | $\begin{gathered} 12 \mathrm{~L} \\ \text { (degres) } \end{gathered}$ | CONVENTIONAL | 20 | 56,120 | 12,310 | 0,263 |
|  |  | LASER | 20 | 56,270 | 12,330 |  |
| 䔍 | HL (mm) | CONVENTIONAL | 20 | 6,490 | 1,080 | 0,012* |
|  |  | LASER | 20 | 6,630 | 1,030 |  |
|  | $\begin{gathered} \overline{\mathrm{LL}} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 12,610 | 1,300 | 000 |
|  |  | LASER | 20 | 12,190 | 2,790 |  |

Table 8. Statistical parameters of AE measurements on third section, left ( $N$-number of
specimens; SD-standard deviation: D -p value: 11 -AE inclination, first method; 12 -AE inclination, specimens; SD -standard deviation; $p-\mathrm{p}$ valu;; $11-\mathrm{AE}$ inclination, first method; $12-\mathrm{AE}$ inclination
second method; $\mathrm{H}-\mathrm{AE}$ height, $\mathrm{L}-\mathrm{AE}$ curved line lengt, L -居t side).

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | I1L (degres) | CONVENTIONAL | 20 | 36,800 | 4,710 | 0,503 |
|  |  | LASER | 20 | 36,720 | 4,720 |  |
|  | $\begin{gathered} \text { I2L } \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 60,140 | 12,260 | 0,115 |
|  |  | LASER | 20 | 60,580 | 12,230 |  |
|  | $\begin{gathered} \mathrm{HL} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 7,560 | 0,980 | 0,263 |
|  |  | LASER | 20 | 7,600 | 1,030 |  |
|  | $\begin{gathered} \hline \mathrm{LL} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 13,480 | 1,630 | 0,503 |
|  |  | LASER | 20 | 13,530 | 1,590 |  |

Table 9. Statistical parameters of AE measurements on fourth section, leff ( $N$-number of
specimens; SD-standard deviation specimens; SD-standard deviation; $p-\mathrm{p}$ value; 11 -AE inclination, first method; 12 -AE inclination E height, L-AE curved line lonet L-bet side)

| z | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11L (degrees) | CONVENTIONAL | 20 | 35,980 | 4,360 | 0,263 |
|  |  | LASER | 20 | 36,110 | 4,190 |  |
|  | $\begin{gathered} 12 \mathrm{~L} \\ \text { (degres) } \end{gathered}$ | CONVENTIONAL | 20 | 61,180 | 10,780 | 0,815 |
|  |  | LASER | 20 | 60,990 | 10,760 |  |
|  | HL (mm) | CONVENTIONAL | 20 | 7,410 | 0,880 | 0,815 |
|  |  | LASER | 20 | 7,500 | 0,910 |  |
|  | LL (mm) | CONVENTIONAL | 20 | 13,530 | 1,120 | 0,115 |
|  |  | LASER | 20 | 13,650 | 1,210 |  |

Table 10. Statistical parameters of AE measurements on fitth section, left ( $N$-number of specimens; SD-standard deviation; $p-p$ value; $11-A E$ inclination, first method; $12-A E$ inclination, second method; $H$-AE height, L-AE curved line lengh, L-efft side),

|  | Variables |  | N | Mean | SD | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | I1L (degrees) | CONVENTIONAL | 20 | 36,020 | 6,070 | 0,003* |
|  |  | LASER | 20 | 36,320 | 5,980 |  |
|  | $\begin{gathered} \mathrm{I2L} \\ \text { (degrees) } \end{gathered}$ | CONVENTIONAL | 20 | 58,500 | 12,750 | 0,263 |
|  |  | LASER | 20 | 58,150 | 11,850 |  |
|  | HL (mm) | CONVENTIONAL | 20 | 6,790 | 9,400 | 1,000 |
|  |  | LASER | 20 | 6,760 | 1,090 |  |
|  | $\begin{gathered} \hline \mathrm{LL} \\ (\mathrm{~mm}) \end{gathered}$ | CONVENTIONAL | 20 | 12,070 | 1,380 | 0,824 |
|  |  | LASER | 20 | 12,160 | 1,320 |  |

## CONCLUSIONS

Silicone impressions eased the procedure and retained accuracy for AE measurements. Differences for most of the performed measurements by conventional and three-dimensional method were not significant, thus indicating same reliability of the used methods. AE values by „best fit line" method were higher than by „fossa roof-eminence top" method no matter which measuring method was used. These values are more affected by the eminence height thus representing simplified but actual condylar path significant for adjustment of articulators.

